4/PKTS

10 / 523497 DT01 Rec'd PUT/PTC 0 4 FEB 2005

1	Apparatus	and	method for treatment of chemical and	į
	4			

2 biological hazards

4 The present invention relates to an apparatus for the

5 treatment of hazardous materials specifically prions,

6 chemical and biological agents. The invention further

7 relates to a method for using such an apparatus.

8

3

9 The risks associated with contamination caused by

10 chemical and biological agents of various kinds are

11 well known. Medical equipment and surgical instruments

12 are required to be sterilised to eliminate a growing

13 range of infectious agents including more recently

14 prions implicated in new variant Creusfeld Jacob

15 Disease (nvCJD). Proteins exhibit huge variation in

16 structure. However, they are formed in similar ways

17 and thus display certain structural elements and

18 characteristics that are common. The primary structure

- 1 of proteins is determined by the amino acid sequence
- 2 and pendant side groups. The amino acid chains are
- 3 then folded to form various secondary structures
- 4 designated as α -helices or β -sheets. Secondary
- 5 structure is determined by the folding of the amino
- 6 acid chains and interactions between the various side
- 7 groups. Further associations may also form, depending
- 8 on the protein's environment. For example different
- 9 hydrophilic and hydrophobic groups or areas within the
- 10 protein molecule are sensitive to the medium in which
- 11 the molecule may be suspended. The prion protein plays
- 12 an essential role in the pathogenesis of a group of
- 13 sporadic, genetically determined and infectious fatal
- 14 degenerative diseases, referred to as prion diseases,
- 15 or transmissible encephalopathys (TSE's), affecting the
- 16 central nervous system of humans and other mammals.
- 17 The cellular prion protein is encoded with a single
- 18 copy gene, highly conserved across mammalian species.
- 19 In prion diseases this protein undergoes conformational
- 20 changes involving a shift from α -helix to β -sheet
- 21 structure. The structures of the proteins, both native
- 22 and rogue, have been extensively investigated. The one
- 23 of most interest and immediate impact to humans is the
- 24 protein associated with nvCJD. What is unusual about
- 25 the protein that is associated with TSEs is the extreme
- 26 robustness it exhibits. This is thought to be due its
- 27 β -sheet structure. Prions are known to survive
- 28 temperatures in excess of 300 °C. Such proteins thus

3 represent present particular problems in terms of their 1 transmission and destruction. The nvCJD prion is known 2 to have a high affinity for stainless steel and other 3 metals posing significant difficulties for the 4 sterilisation of medical equipment, such as surgical 5 instruments. At the same time, considering hazards 6 unrelated to the medical field, chemical and biological 7 agents, such as those used as weapon materials, pose 8 significant handling and disposal risks. 9 10 For the purposes of the present application, the term 11 "hazardous material" means any organic material that 12 may be inimical to human well being and as such may be 13 classed as a chemical or biological hazard. "Hazardous 14 material" includes, but is not restricted to, viral 15 material, bacterial material, prions, proteins, lipids, 16 chemical and biological agents / material with

17

associated organophosphate bases, organic waste or by-18

products associated with pharmaceutical processes and 19

blood products, and further includes all of said agents 20

in isolation and when found within, on the surface of 21

or bonded to other material, instruments or equipment. 22

The term "target material" is used throughout in 23

reference to a "hazardous material" which is to be 24

treated according to the method of the invention. 25

26

The term "treatment" is used in its broadest form and 27

encompasses the deactivation and destruction of 28

hazardous material. Relatively minor modifications to 29

4

the structure or conformation of a particular agent may 1 be sufficient to render it inactive without the need 2 for the agent to be destroyed or decomposed into 3 constituent elements. 5 While some methods for treating such agents are known, 6 7 these typically involve the use of reagents which are themselves difficult to handle and which have 8 associated safety issues. Fluorine and ozone for 9 example may be effective in catalysing such processes, 10 but create significant handling problems and are not 11 suited to use in an open bath apparatus. Furthermore 12 some prior art processes are required to be carried out 13 at very high temperatures and / or pressures. 14

apparatus used in such processes is necessarily complex 15

16 and expensive in light of the associated handling

difficulties. 17

18

There remains therefore a need for a method for the 19 deactivation or destruction of prions, chemical and 20 biological agents, which is effective, efficient and 21 broadly applicable. There is a particular need for an 22 apparatus and a treatment method that can be used to 23 sterilise or decontaminate equipment and instruments 24 that may have come into contact with hazardous 25 material. The present invention as set out below 26

provides such an apparatus and a method for its use.

5 Accordingly, in a first aspect the present invention 1 provides apparatus for treating hazardous material and 2 for decontaminating items that may have come into 3 contact with such material. 4 In its broadest form such apparatus comprises an operator accessible treatment 5 vessel or chamber and a light source capable of 6 irradiating a catalyst within the treatment vessel or 7 chamber with a predetermined wavelength. 8 9 A first embodiment of the invention provides an 10 apparatus, for batch treatment of hazardous material, 11 comprising a treatment vessel for holding material to 12 be treated; a light source for irradiating the contents 13 of the treatment vessel; circulation or agitation means 14 and progress and / or by-product monitoring means. 15

treatment vessel may comprise a 'glove box' type lid 16 facilitating manipulation of the bath contents by an 17

operator. An automatic light source cut-off may be 18

incorporated in order to enhance operator safety. 19

20

A second embodiment provides an apparatus comprising a 21

treatment vessel having one or more decontamination 22

trays for holding hazardous material or items to be 23

treated, a light source for irradiating the contents of 24

the treatment vessel, medium distribution means for 25

circulating a carrier medium within and / or through 26

the apparatus and by-product monitoring means. 27

6

A third embodiment provides an apparatus comprising a 1 holding tank for holding a carrier medium; a catalyst 2 hopper for holding a catalyst; a mixing vessel for 3 mixing the carrier medium and the catalyst; one or more 4 treatment chambers each having a housing which contains 5 a plurality of treatment beds and a light source; and a б distribution header for controlling the flow of carrier medium and catalyst into the treatment chambers. 8 9 Preferably, each treatment bed comprises means for inducing turbulent flow within the carrier medium 10 flowing therein. 11 12 A second aspect of the present invention provides a 13 method for the deactivation and / or destruction of 14 hazardous material comprising the step of irradiating 15 the hazardous material in the presence of a catalyst 16 with light having a wavelength in the range of 310 nm 17 The method of the invention causes to 400 nm. 18 sufficient chemical modification of the hazardous 19 material so as to deactivate or destroy it. 20 21 Preferably, the catalyst is TiO₂ in either rutile or 22 23 24

anatase form and preferably the method is carried out at ambient temperature (of between about 15 to 35 °C) and pressure (of between about 1 to 5 bar). 25

26

The method may be carried out in any water based 27 carrier medium that is compatible with the target 28 material and catalyst. Preferably the carrier medium 29

7

1 is water. Judicious choice of treatment medium is

- 2 required in order to ensure reliable and effective
- 3 treatment. In particular when considering the
- 4 treatment of objects or instruments contaminated with
- 5 prions for example the physical characteristics of the
- 6 apparatus and method should facilitate a suitable
- 7 reaction interface. This involves consideration of the
- 8 composition and viscosity of the carrier medium and the
- 9 path-length of the apparatus such that the target
- 10 material, catalyst and photons from the light source
- 11 are brought together in a manner suitable to effect
- 12 treatment. It follows that a medium that is relatively
- 13 low in viscosity and has appropriate optical
- 14 characteristics (over the wavelength(s) of the light
- 15 source) is desirable. In other words, the viscosity
- 16 must be such as to allow the bringing together of the
- 17 target material and the catalyst and the configuration
- 18 of the apparatus and the optical characteristics of the
- 19 medium must allow sufficient transmission of light to
- 20 the target / catalyst reaction site.

- 22 Thus, the present invention provides for the treatment
- 23 hazardous material such as prions linked with human or
- 24 animal nvCJD in both α and β forms and for treatment of
- 25 instruments and equipment that may have been
- 26 contaminated with said material. The method, and
- 27 apparatus for implementing it, are also applicable to
- 28 the destruction of chemical agent material, typically

8

- 1 organophosphate based systems, as typified by VX or
- 2 Sarin, but additionally blistering and choking agents
- 3 as typified by Mustard Gas and Tear Gas. Depending
- 4 upon the conditions employed, the invention provides
- 5 for total destruction of some hazardous material by
- 6 breaking it down into its constituent parts,
- 7 principally carbon dioxide, nitrogen, water and
- 8 inorganic salts, or alternatively provides for
- 9 sufficient modification of target materials so as to
- 10 render them inactive. The invention can also
- 11 deactivate or destroy many other biohazards, viral and
- 12 bacteriological material, and many commonly
- 13 industrially produced organic materials. Furthermore,
- 14 the method of the invention can be employed to
- 15 decontaminate materials, equipment, instruments and the
- 16 like which may have come into contact with hazardous
- 17 material.

18

- 19 The method of the invention represents an efficient
- 20 means of deactivating and / or destroying of hazardous
- 21 material under mild conditions on a batch basis.
- 22 Further advantages of the invention are described
- 23 below.

24

- 25 The various aspects of the invention are described in
- 26 detail below with reference to the accompanying
- 27 drawings in which:

9

- 1 Figure 1 shows a first embodiment of an apparatus
- 2 according to the invention;
- 3 Figure 2 shows a second embodiment of an apparatus
- 4 according to the invention;
- 5 Figure 3 shows a third embodiment of an apparatus
- 6 according to the invention; and
- 7 Figures 4 and 5 are more detailed views of the
- 8 treatment chamber of the embodiment shown in Figure 3.

9

- _10_ In the drawings similar reference numerals have been
 - 11 used to designate components common to each of the
 - 12 alternative embodiments.

- 14 In its broadest form the invention provides a
- 15 decontamination method for the treatment of hazardous
- 16 material comprising the step of irradiating the
- 17 hazardous material in the presence of a catalyst, with
- 18 light of a suitable wavelength, to deactivate or
- 19 destroy the target material through photocatalytic
- 20 oxidative processes. In general terms, the apparatus
- 21 of the present invention comprises (i) a treatment
- 22 chamber in which the catalyst and the target material
- 23 may be irradiated with light of a suitable wavelength
- 24 (and energy) and (ii) a light source capable of
- 25 producing the desired wavelength. The light source
- 26 wavelength and intensity may be adjusted to optimise
- 27 the process depending upon the nature of the target
- 28 material and the choice of catalyst. A liquid carrier,
- 29 preferably a water based medium, is used to introduce

10

hazardous material into the treatment chamber for 1 2 irradiation. 3 Without being bound by theory, the invention is 4 considered to be the result of an interaction of light 5 energy (photons), the catalyst and water elements that 6 7 forms hydroxyl radicals which cleave sections of, or links in, molecules of the target material ('primary 8 effects'). The action of UV light contributes directly 9 to the breakdown of target materials through photolysis 10 of molecules present. In conjunction with the 11 12 formation of hydroxyl radicals hydrogen peroxide (H2O2) is also produced. This oxidising agent assists and 13 speeds the decontamination process cycle. The primary 14 15 effects of hydroxyl radicals allow secondary processes (such as attack by H₂O₂) to act upon vulnerable parts of 16 the molecules. The ultimate result is the break down 17 of hazardous material into simple (safe) moieties, 18 formation of inorganic salts within the carrier medium 19 and production of off-gases, such as CO2. 20 21 The method of the invention employing highly reactive 22 hydroxyl radicals and H₂O₂ produced through irradiation 23 of a suitable catalyst can be utilised to oxidise prion 24 25 proteins decomposing them to NOx, CO2, water and various inorganic salts. Attack on a prion protein molecule by 26 a hydroxyl radical causes selective breakage of 27 28 multiple bond linkages, thus permanently altering the

crucial relationship between amino acid units and

11

inducing changes to their proper attachment and 1 alignment to each other (and to associated components 2 such as carbohydrates and possibly lipids). 3 4 effect changes the spatial configuration of the prion protein impacting upon its ability to reproduce 5 properly. It is possible that even small alterations 6 in the protein composition and / or configuration are 7 sufficient to impede biological activity of a prion molecule. Any alteration in the structural make-up and 9 configuration reduces the resistance of the prion to 10 further oxidative processes, such as attack by H2O2, 11 thus increasing the rate of complete oxidation of the 12 molecule. 13 14 Contact between the hydroxyl radical / hydrogen 15 peroxide production interface and the target material 16 on the equipment / instruments or the like, using the 17 water based carrier medium with the catalyst, is 18 maximised. This may be addressed by ensuring that the 19 catalyst within the water carrier is migrated to the 20 interface using suitable circulation or entraining 21 processes. Minimising the spatial offset in this 22

manner increases the effects of the short-lived

catalytic particulate (3 - 5 microns).

radicals produced upon irradiation. Spatial offset

distance is further aided through the use of small

23

24

25

12

1 Prior cleaning of gross material make take place within

- 2 the decontamination train, that minimises the volume of
- 3 material to be decontaminated, and improves throughput.

4

- 5 Increasing the intensity of irradiation and / or
- 6 increasing the surface area of catalyst irradiated can
- 7 increase radical production. Additional catalyst may
- 8 be introduced to speed the process and replace catalyst
- 9 extracted from the waste stream.
- 10 The catalyst may be any photosensitive material, which
- 11 allows, through illumination with light of a suitable
- 12 wavelength, a reaction with the associated hazardous
- 13 material to occur. Suitable catalyst materials include
- 14 for example TiO2, TiO3, ZnO, CdS, CdSe, SnO2, WO3, Fe2O3
- 15 and Ta_2O_5 . An example of a preferred catalyst is TiO_2 .
- 16 Irradiation of the catalyst produces active sites (on
- 17 what is in effect a semiconductor surface) causing
- 18 water absorbed to the surface to be oxidised. Highly
- 19 reactive hydroxyl radicals formed in this manner react
- 20 with (and ultimately decompose) the target material
- 21 present in the system.

- 23 The catalyst may be used in any form that provides
- 24 suitable contact with the target material. For
- 25 example, the catalyst may be dispersed in the carrier
- 26 medium or it may be coated onto or mixed with the
- 27 various materials to be decontaminated or destroyed. A
- 28 catalyst module such as a column or tower coated with

13

catalyst material may be employed. Alternatively, the 1 catalyst may be coated onto internal surfaces of the 2 apparatus, enhancing robustness and self-cleaning 3 4 capability. Recovery of the catalytic material for reuse, increasing efficiency of the process, may be 5 provided for as described below. 6 7 While light in the range of 310 nm to 400 nm is 8 preferred, the wavelength of light employed may vary 9 depending upon the catalyst used, the medium used and 10 the nature of the target material. The wavelength to 11 be used may be selected based on the absorption 12 characteristics of the target material, thus increasing 13 efficiency. As photo-generated hydroxyl radicals are 14 the primary agents responsible for the decontamination 15 / destruction processes various parameters may be 16 changed to optimise the effect upon any given target 17 material. The selected wavelength may be produced for 18 example using a standard mercury lamp in conjunction 19 with a suitable filter. 20 21 The method of the invention degrades target materials 22 ultimately reducing them to simple reaction products 23 such as CO2. The evolution of CO2 or any other reaction 24 product can thus be used to monitor the degree and rate 25 of the process. Suitably off-gas production or target 26 material break down may be monitored using techniques 27 such as Raman spectroscopy, mass spectrometry, in vitro 28

14

tests or other known techniques appropriate to any

2 particular hazardous material.

3

4 Characteristics of the method of the invention are

- 5 detailed in Table 1, together with comparable data for
- 6 various prior art methods. The 'efficiency' values
- 7 indicate the rate and effectiveness of electron
- 8 transfer during the treatment process.

15

Catalyst	Efficiency	Medium	Output	Temp	Pressure	Power
	(eV)		toxicity	(°C)	(bar)	
TiO ₂	3.34	Water	Very low	<36	<10	Low
(present			,			
invention)				,		
Ag (II)*	1.98	Nitric	High	~90	10	High
		acid				
Ruthenium*	1.8	H ₂ SO ₄	High	~90	10	High
Chlorination*	1.3	Water	High	~40	<10	Low
H ₂ O ₂ **	2.00	Water	Low	<36	<10	Low

1

2 <u>Table 1.</u> *Indicates prior art process; **Hydrogen 3 peroxide not a catalyst as such - included 4 for comparison purposes only.

- 6 Prior art methods (other than those detailed in Table
- 7 1) include hydrogenation and methods employing molten
- 8 metals or supercritical water. These additional
- 9 methods all pose significant hazards themselves due to
- 10 the operating conditions required in order to be
- 11 effective (for example, all three require temperatures
- 12 in excess of 600 °C; and hydrogenation and
- 13 supercritical water methods operate at pressures of
- 14 about, or in excess of, 100 bar). Treatment with
- 15 fluorine, possibly the strongest oxidising agent known,
- 16 is also effective, but extremely difficult and
- 17 dangerous to handle.

- 1 The method of the invention provides an effective and
- 2 efficient process for the deactivation and / or
- 3 destruction of hazardous material, on batch or
- 4 continuous basis, while overcoming the shortcomings of
- 5 some prior art methods in terms of operational
- 6 requirements and characteristics. The present
- 7 invention facilitates decontamination treatments to be
- 8 carried out under ambient temperature and pressure
- 9 conditions through a method and apparatus which has
- 10 minimal moving parts, is easy to maintain and operate
- 11 and which is readily scalable.

Class of Compound	Examples				
Alkanes	Methane; pentane; heptane;				
	n-dodecane; cyclohexane, paraffin				
Haloalkanes	mono-, di-, tri-, and				
	tetrachloromethane; dichloropropane				
	Pentachloroethane; di and				
	tribromoethane; 1,2-dichloropropane				
Aliphatic Alcohols	methanol; ethanol; n- and				
-	iso-propanol; butanol; penta-1,				
	4-diol				
Aliphatic	methanoic, ethanoic;				
Carboxylic Acids	trichloroacetic; butyric; oxalic				
Alkenes	propene; cyclohexene				
Haloalkenes	di-, tri- and tetra-chloroethene;				
	hexafluoropropene				
Aromatics	benzene; naphthalene, Tributyl				
	Phosphate				
Haloaromatics	chloro and bromobenzene;				
	chlorobenzenes; halophenols				
Phenols	phenol; hydroquinone; catecol;				
	resorcinol; cresol, nitrophenol				
Aromatic	benzoic; phthalic; salicyclic				
Carboxylic Acids					
Polymers	polyethylene; PVC				
Surfactants	polyethylene glycol; p-nonyl phenyl				
	ether; sodium dodecyl benzene				
	sulphonate; paraxon; malathion				
Herbicides	methyl viologen; atrazine;				
	simazine; bentazon				
Pesticides	DDT; parathion; lindane,				
	monocrotophos				
Dyes	methylene blue; rhodamine B; methyl				
	orange; fluorescein				
Explosives	Trinitrotoluene				
Cyanotoxins	Microcystins, Anatoxin-a				
Bacteria	E.Coli., Serratia marcescens,				
Proteins					

Table 2

18

1 Table 2 lists compounds successfully destroyed using

- 2 the present invention. Tributyl phosphate, appearing
- 3 in the 'Aromatics' class, is a simulant for nerve

4 agents.

5

Material	Concentration (% v/v)	Wavelength (nm)	Time (min)	Efficiency (%)	
Methanol	0.1	385 +/- 10	20	99.5	
Paraffin	0.1	385 + / - 10	40	99.75	
Benzene	0.1	380 + / - 10	60	99.9	

6 Table 3.

7

8 Table 3 details a number of test materials and the

- 9 conditions under which they were treated. In each case
- 10 treatment was carried out at atmospheric pressure and
- 11 at room temperature. The treatment efficiency (which
- 12 in the case of the three test materials corresponds to
- 13 destruction of the compounds in question) was measured
- 14 using spectrophotometric techniques.

- 16 The specific embodiments of an apparatus according to
- 17 the invention described below may each be provided with
- 18 a circulation system, a catalyst feed mechanism, and a
- 19 catalyst recovery system. In addition there may be a
- 20 flushing mechanism to remove excess free catalyst
- 21 deposits from the cleaned instruments or tools and
- 22 materials prior to final removal and drying. Larger
- 23 units having the same basic unit structure may be

19

1 complemented by material towers coated with the catalyst through which the contaminated material in the 2 water-based matrix is allowed to percolate, thus 3 4 increasing exposure of the contaminants to the catalyst 5 and UV sources. 6 Prior cleaning of gross material make take place within 7 the decontamination train, that minimises the volume of 8 material to be decontaminated, and improves throughput. 9 10 A first embodiment of an apparatus according to the 11 invention is shown schematically in Figure 1. 12 apparatus comprises a treatment chamber or bath (1), a 13 light source (2), a circulation pump (3), an off-gas 14 monitor / treatment unit (8), a catalyst recovery 15 system (4) and a holding tank (5). A catalyst hopper 16 (6) and a medium storage unit (7) for storing the 17 catalyst and carrier medium prior to use are also 18 provided. This first embodiment has been designed for 19 small quantity throughput of, for example, surgical 20 instruments for decontamination or for destruction of 21 small quantities of target material. Manual 22 manipulation of items in the treatment chamber may be 23 facilitated through use of a glove-box type lid (9). 24 This apparatus is designed for operation by medical 25 26 staff in for example medical or dental practices. 27 Catalyst material and carrier medium are introduced 28

into the holding tank (5), from the catalyst hopper (6)

20

1 and the medium storage unit (7) respectively, and from

- 2 there into the treatment chamber (1). The catalyst is
- 3 typically suspended in the carrier medium and suitable
- 4 stirring means may be provided in order to ensure that
- 5 suspension is maintained and that the suspension
- 6 circulates within the chamber (1). The contaminated
- 7 equipment or target material (not shown) is placed in
- 8 to the bath; the lid closed and interlocks (not shown)
- 9 engaged before the process commences. In order to
- 10 maintain the catalyst in suspension within the carrier
- 11 medium during the process, the medium is circulated
- 12 through the system by using suitable means. This
- 13 facilitates maximum irradiation of the catalyst
- 14 simultaneously allowing the catalyst particles to
- 15 contact the interface with the target material. A
- 16 circulating pump (3) is used for the removal of
- 17 catalyst via the catalyst recovery system (4) at the
- 18 end of the process run. The catalyst recovery system
- 19 (4), typically takes the form of a cyclone separator.
- 20 The level of catalyst in the system is monitored via
- 21 the process controller (not shown) and adjusted to the
- 22 required level. The carrier medium is circulated
- 23 within the bath (1) during the
- 24 decontamination/destruction process and may be replaced
- 25 or replenished from the medium storage unit (7) or via
- 26 the catalyst recovery system (4). The process
- 27 controller (not shown) is used to monitor the overall
- 28 process, including monitoring off-gas production within
- 29 the off-gas monitor/treatment system (8). The off-gas

21

monitoring system (8) provides the means by which the 1 primary process status is monitored. The destruction 2 of organic elements produces CO2, when no further CO2 3 production is detected the treatment process may be regarded as complete. The residual CO2 given off is 5 collected by use of an active charcoal filter fitted 6 into the off-gas system (8). Sampling can be facilitated in order to allow for conformity in vitro 8 testing, spectroscopic analysis or the like to take 9 place. Once completion of the process has been 10 confirmed the used carrier medium can be disposed of in 11 a recognised manner and the apparatus may be flushed 12 with fresh medium. The flushing process enables all the 13 areas within the apparatus that may have been 14 contaminated by target material to be cleaned, although 15 the system is inherently self-decontaminating. 16 carrier medium within treatment chamber (1) is then 17 topped-up prior to next usage and the medium in the 18 holding tank (7) replaced. While the method of the 19 invention may generally be carried out at, or close to, 20 atmospheric pressure, materials may be passed through 21 the apparatus under higher pressure particularly during 22 catalyst recovery and / or cleaning stages. 23 24 Access to the treatment chamber (1) for this activity 25

26 may be provided by a glove box lid arrangement (9).

27 This allows for function (if necessary), dismantling

28 and scrubbing of instruments or equipment to remove

29 stubborn or hidden contaminants. These are

22

subsequently circulated and destroyed in the treatment 1 chamber during the treatment process. Safety 2 interlocks may be employed to minimise any risks to 3 personnel during operation, particularly when introducing target material in to the apparatus. 5 Switching means are provided for deactivating the light source automatically when the bath lid (9) is opened. 7 8 Prior cleaning of gross material make take place within 9 the decontamination train, that minimises the volume of 10 material to be decontaminated, and improves throughput. 11 12 A second embodiment is shown schematically in Figure 2. 13 This apparatus is designed for use in hospitals or 14 larger clinics with high throughput of surgical 15 instruments for decontamination. It is designed for 16 operation by dedicated staff with training in the 17 decontamination of surgical instruments and equipment. 18 19 The apparatus comprises a treatment chamber (1) having 20 decontamination trays (10) an ultraviolet light source 21 (2) and a medium distribution system (11). Catalyst 22 from the catalyst hopper (6) and / or a catalyst 23 recovery system (4) are introduced into a holding tank 24 The contaminated equipment or product is placed 25 in the decontamination trays (10) and the trays (10) 26

are lowered into the treatment chamber (1). The lid is

allowed to start. In order to maintain the catalyst in

closed and interlocks engaged before the process is

27

28

WO 2004/014437

29

23

PCT/GB2003/003431

suspension within the medium, the medium is circulated 1 2 by means of a circulation pump (3) and a medium distribution system (11) having a plurality of rotating 3 spray heads (not shown). The distribution system (11) 4 creates a pressure jet effect that develops a catalyst 5 laden mist or aerosol within the treatment chamber (1) 6 which facilitates optimum contact / interaction between 7 the UV light, catalyst and target material on the 8 contaminated instruments. The carrier medium drains to 9 the bottom of the treatment chamber (1) where it is 10 collected in a circulation header tank (12) which in 11 turn feeds the circulation pump (3). At the end of the 12 treatment process any excess catalyst is recovered from 13 the medium via a catalyst recovery system (4). As 14 described above, a process control (not shown) is 15 provided to monitor progress of the treatment by means 16 of off-gas monitor / treatment system (8). Upon 17 completion of the treatment process, the lid is 18 removed, trays raised and the decontaminated 19 instruments removed. 20 21 22 The medium, including suspended catalyst, may be

circulated directly through the treatment chamber (1) 23 from the holding tank (5) during the decontamination 24 process or via the catalyst treatment unit (4) during 25 the catalyst recovery cycle. Carrier medium is sampled 26 for conformity / quality maintenance as described in 27 relation to the previous embodiment. The medium level 28 within the circulation header tank (12) is monitored

24

1 prior to and during operation and is topped-up as

2 required.

3

4 The third embodiment, shown schematically in Figure 3

5 with details of the treatment chamber arrangement shown

6 in Figures 4 and 5, is designed for either high or low

7 volume destruction of high level bio-hazards such as

8 chemical or biological agent materials, prion

9 contaminated material or the like (and may be adapted

10 to handle solid, liquid or gas phase hazardous

11 materials). It is envisaged that such a system would

12 be operated in a restricted area by dedicated and

13 suitably trained staff.

14

15 The apparatus comprises a series treatment chambers (1)

16 the number and configuration of which may be adapted

17 depending upon the nature and quantity of material to

18 be treated. The target material in a suitable pre-

19 prepared state is introduced from a target material

20 hopper (13) under control of metering means (14) into a

21 mixing vessel (15). The carrier medium is fed in to

22 the mixing vessel (15) from the circulation header tank

23 (12) by the circulation pump (3) and catalyst is added

24 from a catalyst hopper (6). The pre-treatment

25 preparation of the target material may include but need

26 not be limited to the breaking down of solids into

27 smaller particles, the suspension of solid particles in

28 a liquid or the absorption of a gas into a liquid. The

29 target material, medium and catalyst mixture cascades

25

1 into distribution header (16) from which it enters the

- 2 treatment chambers (1). This method of controlling the
- 3 flow of the mixture removes any potential pressure
- 4 other than the hydrostatic head determined by the
- 5 relationship between the mixing vessel (15) and the
- 6 distribution header (16). Each treatment chamber (1)
- 7 comprises a housing that contains a series of tray-like
- 8 treatment beds and a light source (2). The treatments
- 9 beds are designed to maximise the time which the
- 10 carrier medium, catalyst and target material mixture is
- 11 exposed to the UV light, as well as promoting the
- 12 formation of turbulent flow. Typically each treatment
- 13 bed comprises of a series of channels (17) running back
- 14 and forth across the bed, each channel (17) containing
- 15 a textured surface (18) designed to induce turbulent
- 16 flow within the mixture. Control of the flow in this
- 17 manner prevents the catalyst and target material from
- 18 being shielded (as could occur in a laminar flow
- 19 situation) and maximises irradiation effectiveness.
- 20 The treatment beds are configured with a light source
- 21 (2), optionally shrouded with a mirror, directly
- 22 overhead. Each treatment bed further comprises a
- 23 transparent top plate, typically made from quartz or
- 24 some other material having suitable light transmission
- 25 characteristics. The treatment mixture is circulated
- 26 around the system until the process has been completed
- 27 or for a suitable duration as dictated by the operator.
- 28 Any suspended solids, catalyst and other waste products

26

are removed via a catalyst / waste treatment system (4) 2 for storage prior to final disposal. 3 Specific modifications may be introduced into the 4 carrier medium composition and flow control in order to 5 create the necessary environment for the target 7 material to be suspended within the medium. example, rotary, ultrasonic or other stirring / 8 9 agitation means make be incorporated into the 10 apparatus. 11 12 The process is controlled using a suitable process 13 monitoring and control system. This includes monitoring the off-gas status by means of an off-gas 14 15 monitoring / treatment system (8). The off-gas 16 monitoring / treatment system (8) also provides a means 17 for the monitoring and collection / treatment of 18 gaseous reaction products such CO_2 , NO_x , SO_x and the 19 like. In order to treat these off-gases specific 20 equipment such as scrubbers and absorbers may be provided. As before suitable analytical techniques can 21 be employed to monitor the course of the treatment and 22 the content of used waste products and used carrier 23 24 medium. 25 The invention is not limited to the embodiments herein 26 described which can be varied in construction and 27

28

detail.